



# Residential Footing Design and Reinforcement Quality

© SRIA 2025



### Web Site: sria.com.au

### Information about the SRIA

MEMBER LOGIN



**Our Objectives** 

**NEWS & EVENTS CONTACT** 

**RESOURCES** 

Member Services
Technical Leadership
Codes, Standards and Regulations
Market Development

The Hub for Steel Reinforcement Knowledge and Support

Quality and Traceability
Workplace Health and Safety
Prefabrication
Australian Manufacturing and Jobs
Digital Detailing
Sustainability
One Stop Shop





# Web Site: sria.com.au Has a Wealth of Information



QUALITY CERTIFICATION

MEMBERSHIP

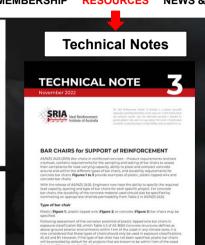
**RESOURCES** NEWS & EVENTS CONTACT

FABRICATION AND SITE HANDLING OF REINFORCING BARS

MEMBER LOGIN















TECHNICAL NOTE



### Web Site: sria.com.au Has a Wealth of Information



ABOUT US QUALITY C

QUALITY CERTIFICATION MEMBERSHIP

RESOURCE

**NEWS & EVENTS** 

CONTAC

MEMBER LOGIN



**Technical Publications** 

**Technical Notes** 

**Construction Tips and Alerts** 

**Conference Papers and Presentations** 

Lectures

Research

**Videos** 

# RAFT SLAB DESIGN AND DETAILING - VICTORIAN STRUCTURAL BRANCH COMMITTEE OF ENGINEERS AUSTRALIA 12 JULY 2016

Title	Description	Size
Presentation by Peter Bayetto	Compliance with AS2870-2011 - Recent Failure Investigations and Design by Engineering Principles (rev	23.1 MB
Presentation by Eric Lume	Residential Slabs and Footings Construction Requirements	6.3 MB
Presentation by Scott Munter	Residential Slabs and Footings Reinforcement and Slab Design	7.3 MB



## Reinforcing Bar Classification

All reinforcing bar to comply with: AS/NZS 4671 Steel for the reinforcement of concrete

AS/NZS 4671 Designation	Yield Stress MPa	Ductility Class	' Description ' '		
S600N	600	N	Hot-rolled Deformed bar	11, 15, 18, 22, 26, 29, 33, 37	
D500N	500	N	Hot-rolled Deformed bar	Coil (10-20), Straight (12-40), Special (50)	
R250N	250	N	Hot-rolled Plain round	6.5, 10, 12, 16, 20, 24	
D250N	250	N	Hot-rolled Deformed bar	12 (pool steel)	
D500L	500	L	Cold-rolled Deformed bar	5 - 12	
R500L	500	L	Cold-drawn Round rod	5 - 12	

#### Symbols used

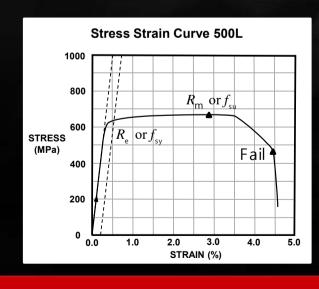
- S Deformed Grade 600 Ductility Class N Bars ie S18
- N Deformed Grade 500 Ductility Class N Bars ie N20
- POL Deformed Grade 250 Ductility Class N Bars ie POL 12
- R Plain Round Grade 250 Ductility Class N Bars ie R10
- L Plain Round Grade 500 Ductility Class L Bars ie L10

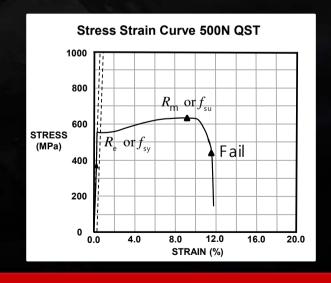


# Mechanical Properties

### AS/NZS 4671:2019 Steel for the reinforcement of concrete: Table 7.2 (A&B)

Property		250N	500L	500N	600N	750N	Probability of exceedance
Nominal Diameter (mm)		12 (pool steel)	5 to 12	10 to 40	10 to 40	8.2, 9.8 & 13	-
Yield Stress (MPa)	R <sub>ek.U</sub>	≥ 250 -	≥ 500 ≤ 750	≥ 500 ≤ 650	≥ 600 ≤ 750	≥ 750 ≤ 900	$C_{\text{vL}}$ : $P = 0.95$ $C_{\text{vU}}$ : $P = 0.05$
Ratio	$(R_{\rm m}/R_{\rm e})_{\rm k.L}$	≥ 1.08	≥ 1.03	≥ 1.08	≥ 1.08	≥ 1.04	$C_{\rm vL}$ : $P = 0.90$
Uniform Elongation (%)	A <sub>gt.k.L</sub>	≥ 5.0	≥ 1.5	≥ 5.0	≥ 5.0	≥ 4.0	$C_{\rm VL}$ : $P = 0.90$







# **Chemical Composition**

	Chemical Composition (%) Max							
Type of analysis	С		Р	S	Carbon Equivalence Value for Class			
	500L 500N	600N 750N	All steel grades		500L	500N	600N & 750N	
Cast analysis	0.22	0.33	0.050	0.050	0.39	0.44	0.49	
Product analysis	0.24	0.35	0.055	0.055	0.41	0.46	0.51	



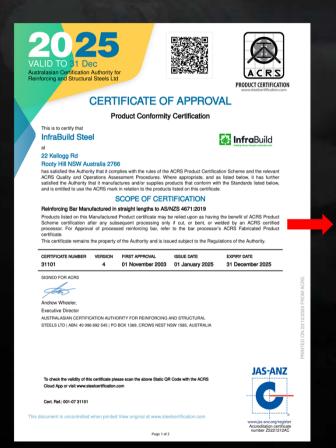
### **Carbon Equivalence:**

$$C_{\text{eq}} = C + \frac{Mn}{6} + \frac{Cr + Mo + V}{5} + \frac{Ni + Cu}{15}$$

**Correct chemistry allows** welding to AS/NZS 1554.3



### **JASANZ Accredited Third Party Certification**



**Example of a JASANZ Accredited 3<sup>rd</sup> Party Mill Certificate** 

Certifies the stock bar, rod and coiled products conform to AS/NZS 4671

Straight Bar Manufactured to AS/NZS 4671:2019
Manufactured Bars listed on the ACRS Certificate,
only remain ACRS Certified if cut, or bent, or welded
by an ACRS certified processor.

For Approval of processed reinforcing bar, refer to the bar processor's ACRS Fabricated Product certificate.

JASANZ
Joint Accreditation System of
Australia and New Zealand



### **Need for a JASANZ Accredited Third Party Certificate**

Every project should specify one and obtain to guarantee quality





# Ensuring Quality Reinforcement JASANZ Accredited 3<sup>rd</sup> Party Processor Certificate

Required by purchasers to prove quality reinforcement delivered to site







#### CERTIFICATE OF APPROVAL

Product Conformity Certification

#### Certificate No: 811021

Ausreo Pty Ltd

Gate C, 133/139 Newton Rd Wetherill Park NSW Australia 2164



#### Products assessed by ACRS to the following Standards:

- Processing and distribution of Grade 250N and 50N carbon steel bars and welded mesh in accordance with ASINZS 4617; 2019, and either AS 3690: 2018 Concrete structures and AS 5100.52: 2017 Bridge design – Concrete "material and construction requirements for reinforcing steel", or the "Reinforcement" clauses of NZS 3109 Concrete Construction.
- Threading of reinforcing bar for the application of a Lenton Coupler with equipment, training and maintenance provided by the supplier.

Processed steel reinforcing materials may only be relied upon as having the benefit of ACRS Product Scheme certification when manufactured or processed by ACRS certificate holders.

#### Approved Company Information

Tag



To check the validity of this certificate please scan the above Static QR Code with the ACRS Cloud App or visit www.steelcertification.com

Cert. Ref.: 021-01 8110

This document is uncontrolled when printed View original at www.steelcertification.co



ACRS Processor Certificate only available if reinforcement supplied by ACRS Certified Mill

Processing of Grade 250N and 500N carbon steel bars and welded mesh in accordance with AS/NZS 4671 (2019) and either:

- · AS 3600 (2018) Concrete structures
- AS 5100.5 Bridge design Concrete
- NZS 3109 Concrete Construction



# **Bending Reinforcement**

Clause 17.2.3.2 of AS 3600 - required pin diameters

Avoids excessive steel strain and crushing of concrete

### **Fitments**

500L & R250N

D500N

### **General**

**D500N** 

Galvanised ≤16mm

Galvanised ≥ 20mm

3*d*<sub>b</sub>

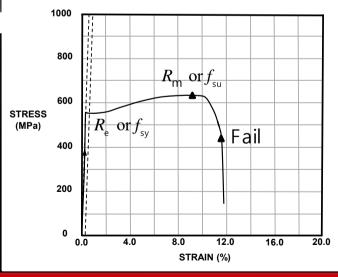
 $4d_{\rm b}$ 

 $5d_{\rm b}$ 

 $5d_{\rm b}$ 

 $8d_{\rm b}$ 











**Need for a JASANZ Accredited Third Party Certificate** 

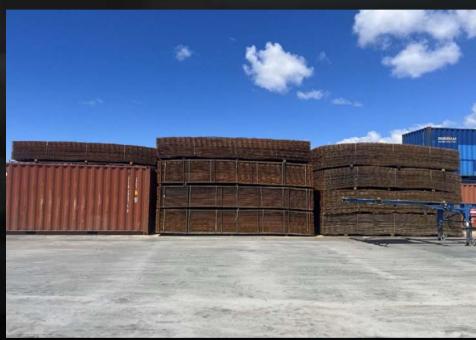
Every project should specify one and obtain to guarantee quality





Recent increase in imported mesh product







# SRIA Industry Warning late 2023

For updates connect with SRIA on social media: LinkedIn Facebook Instagram



Imported NON-COMPLIANT STEEL MESH is being sold to unsuspecting customers

The unique markings on the longitudinal and crossbars of the mesh do not match the markings on the quality certificate sent to the customer.

#### Two options to protect yourself:

1. Verify the markings on the mesh MATCH the markings on the certificate.

If they don't match, return the mesh to the supplier as non-conforming product.



Click to view certification

2. Buy steel mesh from a SRIA member.

ALL SRIA members hold current JASANZ accredited 3rd party certification to prove their mesh conforms to AS/NZS 4671.

Click to view our members

Since 1988, it's been our duty to support reinforcing steel quality and capability in Australia. Don't take the risk of having to replace the building or structure because you used non-conforming steel mesh.



sria.com.au

NON - CONFORMING MESH CAMPAIGN RAISING AWARENESS ON SOCIAL MEDIA



David Chandler OAM . Following

NSW Building Commissioner at NSW Department of Customer Service

#BuildingCommissionNSW will be keeping an eye out. #Engineers #Certifiers #Builders expect check-ups of #OccupationCertificates and on-site. Will be an avoidable tragedy to have to demolish slabs if found. Be assured if counterfiet products are discovered they will be coming out. #BuildingCompliance #Accountability #Licences #Risk



Like · €€ 84 Reply · 8 Replies



### Products found accompanied with false ACRS Certificates

- Always check Certificates on JASANZ website
- This company (logo removed) was a non-Australia producer for >10 years
- Printed copies may have been altered
- SRIA Member's Certificates can be found on SRIA website

Philip Sanders resigned as Executive Director some years prior to this Certificate





On Site – check that bar markings match the JASANZ 3rd party Certificate

Bar marking



ACRS Certificate for imported mesh





Tag on mesh?





### ACRS Certificate updated after questions raised

- Bar marking now matches 'interim' 2023/2024 image
- Always buy from a JASANZ 3<sup>rd</sup> party accredited mill for traceability

















To check the validity of this certificate please scan the above Static QR Code with the ACRS Cloud App or visit www.steelcertification.com

Cert. Ref.: 082-01 160802 4

This document is uncontrolled when printed View original at www.steelcertification.co

Page 2 of 2

www.jas-anz.org/re-Accreditation certif number Z5221213

Cloud App or visit www.steelcertification.com

Cert. Ref.: 082-01 160802 4

Either: 1. Buy from an SRIA Member – All JASANZ accredited 3rd Party Certified

- Obtain JASANZ accredited 3<sup>rd</sup> Party Mill & Processor Certificates
   Check that Certificates are authentic
   (register.jasanz.org/certified-organisations and search for AS/NZS 4671)
- 3. Ensure tags/bar markings match the Certificate when inspecting





### Surface Condition of Reinforcement

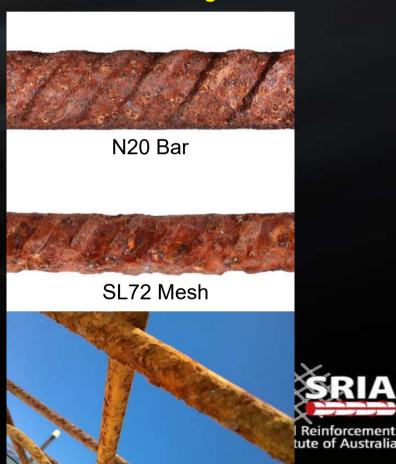
### Ensure no loose or flaking rust on surface of bar

- Indicates loss of steel section (or mass) which may affect performance
- Limits on mass provided in Table 7.5 (A) of AS/NZS 4671
- **▶** If outside these limits, then non-conforming
- Refer also SRIA Technical Note 1

### **Acceptable – surface corrosion**



# Unacceptable Loose and flaking rust



# Bending Reinforcement on Site

Incorrect Site Practices

### Not bending around correct pin diameter

- Site rebending now covered by Clause 17.2.3.2 of AS 3600 (2018) due to poor site practices
- Use of pipes for leverage no longer allowed in AS 3600 due to a lack of control on site
- Refer also SRIA Technical Note 4







# Bending Reinforcement on Site Recommend bars bent properly by Processor

Take care in approving site bent reinforcement



Bends up to 180

Maximum D16 bar

35 - 63 mm bending roller

Depends on brand and model



Bends of 90, 135 and 180 Max D20 bar Roller diameter?





Bends 45, 90, 135 & 180 Roller 38, 50 & 62 Max N20 bar







# Mesh Processing

### Quality of welding and adequate lap are critical

- Each welded joint develops50% of the bar's yield stress
- Clause 7.2.5 of AS/NZS 4671



Overlap mesh sheets a minimum of 2 cross-bars

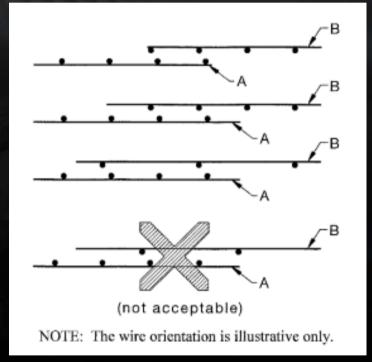


Figure 6.5 of CIA Handbook Figure 5.1 from AS 2870



Overlap mesh sheets a minimum of 2 cross-bars



Note: Concreter on project taught to overlap mesh by 125 mm

have been here



### National Construction Code Requirements

### **Performance Requirements**

#### H1P1 Structural reliability and resistance

[2019: P2.1.1]

- (1) By resisting the actions to which it may reasonably be expected to be subjected, a building or structure, during construction and use, with appropriate degrees of reliability, must—
  - (a) perform adequately under all reasonably expected design actions; and
  - (b) withstand extreme or frequently repeated design actions; and
  - (c) be designed to sustain local damage, with the structural system as a remaining stable and not being damaged to an extent disproportionate to the original local damage; and
  - (d) avoid causing damage to other properties.



### National Construction Code Requirements

### **NCC Performance requirements**

- (2) The actions to be considered to satisfy (1) include but are not limited to—
  - (a) permanent actions (dead loads); and
  - (b) imposed actions (live loads arising from occupancy and use); and
  - (c) wind action; and
  - (d) earthquake action; and
  - (e) snow action; and
  - (f) liquid pressure action; and
  - (g) ground water action; and
  - (h) rainwater action (including ponding action); and
  - (i) earth pressure action; and
  - (j) differential movement; and
  - (k) time dependent effects (including creep and shrinkage); and
  - (I) thermal effects; and
  - (m) ground movement caused by—
    - (i) swelling, shrinkage or freezing of the subsoil; and
    - (ii) landslip or subsidence; and
    - (iii) siteworks associated with the building or structure; and
  - (n) construction activity actions; and
  - (o) termite actions.



### National Construction Code Requirements

### **NCC Performance requirements**

- (3) The structural resistance of materials and forms of construction must be determined using five percentile characteristic material properties with appropriate allowance for—
  - (a) known construction activities; and
  - (b) type of material; and
  - (c) characteristics of the site; and
  - (d) the degree of accuracy inherent in the methods used to assess the structural behaviour; and
  - (e) action effects arising from the differential settlement of foundations, and from restrained dimensional changes due to temperature, moisture, shrinkage, creep and similar effects.

#### H1D1 Deemed-to-Satisfy Provisions

[New for 2022]

- (1) Where a *Deemed-to-Satisfy Solution* is proposed, *Performance Requirements* H1P1 and H1P2 are satisfied by complying with H1D2 to H1D11.
- (2) Where a *Performance Solution* is proposed, the relevant *Performance Requirements* must be determined in accordance with A2G2(3) and A2G4(3) as applicable.



# AS 2870 Section 1: Scope and General

#### 1.2 APPLICATION

To comply with this Standard:

- (a) all sites shall be classified in accordance with Section 2; &
- (b) footing system design shall be performed by either:
  - (i) prescribing a standard design in accordance with Section 3; or
  - (ii) applying the engineering principles described in Section 4; &
- (c) all design and construction shall comply with Sections 5 and 6.

Residential concrete footing system design, detailing and construction should also comply with AS 3600, except that if in conflict, AS 2870 takes precedence.



# AS 2870: Design Process



Residential Building

### Footing System ("barrier"):

- Standard Designs (SECTION 3)
- Design by Engineering Principles (SECTION 4)
- //////////////////////////////Foundation:

• Site classification (Section 2)



- DTS Designs calibrated empirically by observing the real performance and reserve strength of completed buildings.
- Less emphasis on design loads & greater emphasis on foundation movement
- Clause 1.4.2 design actions are:
  - $\rightarrow$  1.0 × Foundation movement + 1.0 × Permanent action (DL) + 0.5 × Imposed action (LL)
- Why this design philosophy?
  - ➡ Foundation movement is a primary design consideration for footing systems which act as a "barrier" to protect the structure they support.
  - ▶ Less emphasis given to dead and live loads reduces overall cost of housing nationally.
  - Failure due to overloading poses only a minimal or nonexistent risk to life.
- The minimum requirements will not necessarily result in a defect-free building, as stated in Clause 1.3.1.

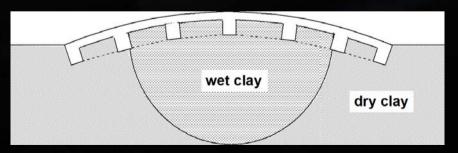


		Edge and internal beams					
Site class	Type of construction	Depth	Bottom re	einforcement	Top bar	Max beam	
		(D) mm	Mesh	Bar alternative	reinforcement	spacing cc m	
Class A	Clad frame	300	3-L8TM	2N12	-	-	
	Articulated masonry veneer	300	3-L8TM	2N12	100	-	
	Masonry veneer	300	3-L8TM	2N12	100	100	
	Articulated full masonry Full masonry	400 500	3-L8TM 3-L8TM	2N12 2N12		1	
Class S	Clad frame	300	3-L8TM	2N12	100	-	
	Articulated masonry veneer	300	3-L8TM	2N12	100	7	
	Masonry veneer	300	3-L11TM	3N12	20142	1	
	Articulated full masonry	500	3-L11TM	3N12	2N12	į.	
	Full masonry	700	2x3-L11TM	3N16	2N16	5	
Class M	Clad frame	300	3-L11TM	3N12	-	6	
	Articulated masonry veneer	400	3-L11TM	3N12	-	6	
	Masonry veneer	400	3-L11TM	3N12		5	
	Articulated full masonry	625	3-L11TM	3N12	2N12	4	
	Full masonry	950	2x3-L11TM	3N16	2N16	4	
Class M-D	Clad frame	400	3-L11TM	3N12	-	5	
	Articulated masonry veneer	400	3-L11TM	3N12	1N12	4	
	Masonry veneer	500	3-L12TM	3N12	2N12	4	
	Articulated full masonry	650	3-L11TM	2N16	2N16	4	
	Full masonry	1050	2x3-L11TM	3N16	3N16	4	
Class H1	Clad frame	400	3-L11TM	3N12	-	5	
	Articulated masonry veneer	400	3-L11TM	3N12	1N12	4	
	Masonry veneer	500	3-L11TM	3N12	3N12	4	
	Articulated full masonry	750	2x3-L11TM	3N16	2N16	4	
	Full masonry	1050	2x3-L12TM	3N16	3N16	4	
Class H1-D	Clad frame	400	3-L11TM	3N12	1N12	4	
	Articulated masonry veneer	500	3-L11TM	3N12	2N12	4	
	Masonry veneer	650	2x3-L11TM	3N16	1N16	4	
	Articulated full masonry	800	2x3-L11TM	3N16	2N16	4	
	Full masonry	1100	2x3-L12TM	3N16	3N16	4	
Class H2	Clad frame	550	3-L11TM	3N12	2N12	4	
	Articulated masonry veneer	600	3-L12TM	3N12	2N12	4	
	Masonry veneer	750	2x3-L11TM	3N16	2N16	4	
	Articulated full masonry	1000	2x3-L11TM	3N16	2N16	4	
	Full masonry	-	100	-		-	
Class H2-D	Clad frame	550	2x3-L11TM	3N16	2N16	4	
	Articulated masonry veneer	700	2x3-L11TM	3N16	2N16	4	
	Masonry veneer	750	2x3-L11TM	3N16	2N16	4	
	Articulated full masonry	1000	2x3-L11TM	3N16	2N16	4	
	Full masonry	-	4.0	-	100	-	
	Articulated full masonry	1000				4	

Standard Designs - Figure 3.1 (in part)

- Section 3 Deem-to-comply 'recipe' footing system designs cover most sites (except Class E & P)
- Maximum differential footing deflection (i.e. serviceability) is specified for the design of footing & rafts in Table 4.1
- Limits damage depending on sensitivity and type of supported elements e.g. masonry.
- Slabs & footings modelled as beams or rafts supported on a foundation are indeterminate systems.
- Software is an efficient modelling tool and has been used to check
   Section 3 design models to Section 4 engineering principles.
- One such program is 'CORD' Code Orientated Raft Design, a commercial footing design program.







Standard reinforcement designs satisfy the following criteria (of Section 4):

**BENDING STRENGTH (cross-section design): Clause 4.4 (f)** 

- $M^* \leq \phi M_u$ 
  - $ightharpoonup M_{\rm u}$  = nominal moment capacity calculated in accordance with AS 3600, e.g.  $f_{\rm sv}$ =500 MPa
  - $\phi$  = capacity reduction factor (NOTE:  $\phi$  = 0.85 for both Class L & N steels in AS 2870)

### SHEAR STRENGTH (region design, e.g. punching shear): Clause 4.4 (j)

- $V^* \leq \phi V_u$ 
  - $V_u$  = nominal shear capacity (with or without shear reo) calculated in accordance with AS 3600
  - $\phi$  = capacity reduction factor ( $\phi$  =0.7 for both Class L & N steels)

### **DUCTILITY (overall member design): Clause 4.4(i)**

- $M_{\rm u} \ge 1.2 M_{\rm cr}$  (minimum bending strength for multiple crack development)
  - flexural cracking moment,  $M_{cr}$  (for  $f'_{c}$ = 20 MPa : sagging  $f_{t}$  = 2.7 MPa; hogging  $f_{t}$  = 1.8 MPa)

### **NOTE:** All standard footing designs developed with:

 $\phi$  = 0.85 (flexure) or 0.7 (shear) for Ductility Class L & N steels.



# Mixing Ductility Class L & N Steels

If mixing Ductility Class L & N steels together in a single layer, for AS 2870 footing designs they are treated as fully equivalent:

- $\phi$  = 0.85 to calculate  $\phi M_{II}$ 
  - → Moment redistribution is not normally assumed when calculating M\*, which reduces ductility demand on the reinforcing steel
  - No imminent warning requirements
  - Sections normally under-reinforced
  - When calculating nominal moment capacity,  $M_{\rm u}$ , assume all steel is at yield stress,  $f_{\rm sv}$  = 500 MPa
- $\phi$  = 0.7 to calculate  $\phi V_u$ 
  - When calculating nominal shear capacity excluding contribution of shear reinforcement, V<sub>uc</sub>, for example, all fully-anchored Class L & N main bars are fully effective, i.e. use full cross-sectional area.



Class N bars and Class L mesh effectively in a SINGLE LAYER

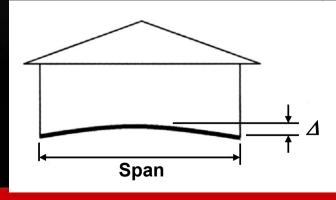


Greatest ductility demand is in Clad or Articulated Masonry Veneer

Maximum Design Differential Footing Deflection for Design of Footings and Rafts (Table 4.1)

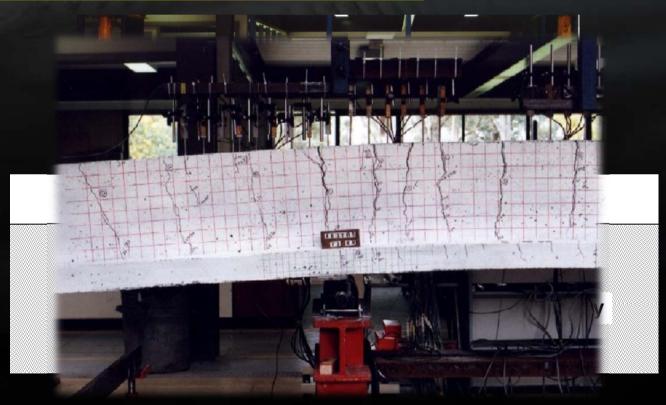
Type of construction	Maximum differential deflection, as a function of span, mm	Maximum differential deflection, mm
Clad Frame	L/300	40
Articulated masonry veneer	L/400	30
Masonry veneer	L/600	20
Articulated full masonry	L/800	15
Full masonry	L/2000	10

NOTE: Deeper (stiffer) members are required as the design differential deflection reduces. Their ductility is less, but so is the ductility demand.





These deformations can be accommodated by the ductility of the reinforced-concrete sections incorporating either Class L or N reinforcing steel provided they are designed for multiple cracking.





### AS 2870 Section 4: Modification of Standard Design

Clause 4.1 GENERAL: "This Section may be used to extend the range of validity of, or modify, the deemed-to comply designs contained in Section 3..."

# Simplified Method (Clause 4.5) Design parameters within the following range (Clause 4.5.1)

Design Parameter	Range
y <sub>s</sub>	10 mm to 70 mm if $H_{\rm s}$ > 3 m or 10 mm to 100 mm if $H_{\rm s}$ < 3 m
Δ	5 mm to 50 mm
Span	5 m to 30 m
Beam spacing	≤ 1.25 values in Figure 3.1 Clause 5.3.9 shall apply at external corners of the building. For Class E sites the beam spacing shall not exceed 5 m.
Beam depth	250 mm to 1200 mm
Minimum depth of any beam	≥ 0.8 max. beam depth
Beam width	110 mm to 400 mm
Design distributed load	≤ 10 kPa
Design edge line load	≤ 25 kN/m



# AS 2870 Section 4: Design by Engineering Principles

Clause 4.5.2: "...strength shall be provided by the satisfaction of the ductility requirements of Clause 4.4(i)"

#### **Ductility Requirements & Durability:**

- Satisfying the ductility requirement  $M_u \ge 1.2 M_{cr}$  allows multiple cracks to form over any zone under a high degree of bending.
  - Concrete block elements form between adjacent cracks, spaced approximately D apart, providing a mechanism for greater overall member deformation
- Multiple cracking in peak moment regions avoids concentrating the crack width at the firstcracked section.
  - ▶ With 3-4 cracks forming in each peak region, more rotation is achieved as demanded by the soil movement, etc., and finer cracks normally maintain durability
  - e.g. 1 crack 0.6 mm wide can be visually a problem, damage finishes or be a corrosion issue, while 3 fine cracks each 0.2 mm wide is good design.
- Class L and N reinforcing steels complying to AS/NZS 4671 have sufficient ductility to ensure adequate deformation capacity.



## AS 2870 Section 4: Design by Engineering Principles

#### **Reinforcement Requirements for Higher Concrete Grade:**

- Standard Section 3 footing designs are all based on  $f'_c$  = 20MPa and do not apply for concrete grades of 32 MPa or greater.
- Higher grade concretes may be required e.g. saline conditions.
- Tensile strength and modulus of elasticity will both increase in proportion to the square root of compressive strength grade,  $f'_c$ .

Concrete grade	Modulus of elasticity E MPa	Tensile strength Hogging deformation MPa	Tensile strength Sagging deformation MPa
N20	15000	1.8	2.7
N25	16800	2.0	3.0
N32	19000	2.3	3.4
N40	21200	2.5	3.8

 If concrete sections remain unchanged, then designers must calculate the steel reinforcement required to satisfy ductility,



## Importance of Site Inspections



- Approval of engineering design & specification requirements.
- Ensure quality materials used
- Site inspection is essential before any concrete placement.
- Take photographs and watch start of a concrete pour if there are concerns.





## Industry Issues Identified with AS 2870

#### **Proposed revision of AS 2870 (2011)**

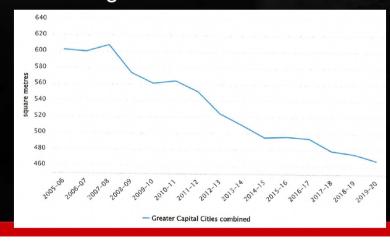
To address problem areas identified since 2011 revision, including:

- Footing performance
- Normal and abnormal sites (weather + zero lot alignments)
- Site classification impacts of construction
- More guidance for Class P sites
- Guidance for concrete strengths > 25 MPa
- Include high strength reinforcement
- Review reinforcement detailing requirements
- Review plumbing requirements
- Designing for trees (currently informative Appendix)



#### **Normal and Abnormal Sites**

- Add new abnormal moisture conditions
- Condition identifying and treating initially desiccated sites
- Zero lot alignment sites
- Smaller lot sizes
- Requirement for trees
- Site classification P
- More guidance for Class P sites









#### **Site Classification**

- Undertaken by suitably qualified people
- More reliable classification in difficult or non-standard conditions
- Currently number of boreholes not specified
- Extent of investigation not covered
- Tree removal during land development (use satellite imagery)
- Basements
- Changes to classification if backfill and drainage not adequate





#### **Guidance for Class P Sites**

- Currently no guidance provided
- Guidance will provide more standard approach
- Reduce the number of sites outside scope of Standard
- Provide more economical footing designs for Class P sites

#### **Concrete Strengths > 25 MPa**

If concrete strength > 25 MPa

- → Ductility requirements of Clause 4.4(i) need to be satisfied
- Provide additional Tables to cover 32 MPa and 40 MPa concretes

#### **High Strength Reinforcement**

Include use of 600 MPa reinforcement



#### **Plumbing Requirements**

- Review existing requirements for flexible connections
- Consider encasement for Class E
- Ensure consistency with plumbing Standard

#### **Designing for Trees**

- Trees and reduced boundary distances
- Normal and abnormal sites (weather and zero lot alignments)





#### **Reinforcement Detailing Requirements**

Items to be reviewed and/or included:

- Mesh lapping requirements
- Ensure edge bar located along slab edges
- Bending of reinforcement on site (Tech Note 4)
- Surface condition of reinforcement (Tech Note 1)
- Lap lengths (Tech Note 7)
- Cover set using bar chairs
- Include AS/NZS 2425 reference
- Bar chair spacing (Tech Note 3)

















SRIA website provides links to industry at SRIA.COM.AU

**Full Processor Members >10 years of membership** 























**Ordinary Processor Members <10 years of membership** 







## **SRIA Associate Members**

**ACCESSORY SUPPLIERS - Links to suppliers at SRIA.COM.AU** 

































## SRIA Associate Members - Machinery

MACHINERY SUPPLIERS
Links to suppliers at SRIA.COM.AU



















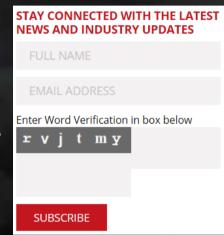




## **Stay Connected**

#### Register on SRIA web site

- Newsletter
- Latest Publications
- Seminars and Conferences
- Industry News



#### Follow us on



Link on web site



Free bar and mesh gauges (order on web site)





## SRIA Disclaimer

The information presented by the Steel Reinforcement Institute of Australia in this publication has been prepared for general information only and does not in any way constitute recommendations or professional advice. While every effort has been made and all reasonable care taken to ensure the accuracy of the information contained in this publication, this information should not be used or relied upon for any specific application without investigation and verification as to its accuracy, suitability and applicability by a competent professional person in this regard. The Steel Reinforcement Institute of Australia, its officers and employees and the authors and editors of this publication do not give any warranties or make any representations in relation to the information provided herein and to the extent permitted by law (a) will not be held liable or responsible in any way; and (b) expressly disclaim any liability or responsibility for any loss or damage costs or expenses incurred in connection with this publication by any person, whether that person is the purchaser of this publication or not. Without limitation, this includes loss, damage, costs and expenses incurred as a result of the negligence of the authors, editors or publishers.

The information in this publication should not be relied upon as a substitute for independent due diligence, professional or legal advice and in this regards the services of a competent professional person or persons should be sought.



## Thank you









# Residential Slabs and Footings Detailing and Construction Requirements

© SRIA 2025



## **Problem or Performance**

The most controversial aspect of AS 2870 is almost certainly that some damage may occur even though all parties have fulfilled their obligations competently.

- Some factors unknown even after detailed investigation
- Compromise between cost and reasonably foreseeable actions
- Standard designs not expected to fully resist all actions
- → Homeowners may request more conservative design

#### Clause 1.4.3

The design of footing systems shall consider the following:

- (a) Effective drainage of the site
- (c) Control, but not prevention, of shrinkage cracking
- (d) Control, but not prevention, of cracking due to footing movement
- (e) Stiffness and ductility of the footing system
- (g) Tolerance of the wall system to movement

Comply with AS 2870 and NCC wherever possible



## Performance - Site Investigation

#### **Number of boreholes required**

- Minimum one borehole or pit per building site, or site of extension
- Minimum three boreholes per site if soil known to be highly variable, or  $H_s \ge 3.0 \text{ m}$
- → Number across housing subdivision may be reduced if consistent



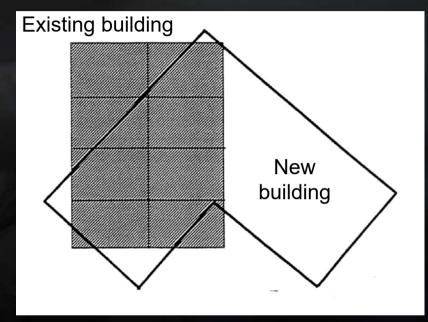






## **Abnormal Moisture Conditions**

- Drains
- → Channels
- Ponds
- Dams
- → Tanks
- → Trees
- **→** Fill
- Urbanisation
- Previous structures
- Onsite wastewater disposal

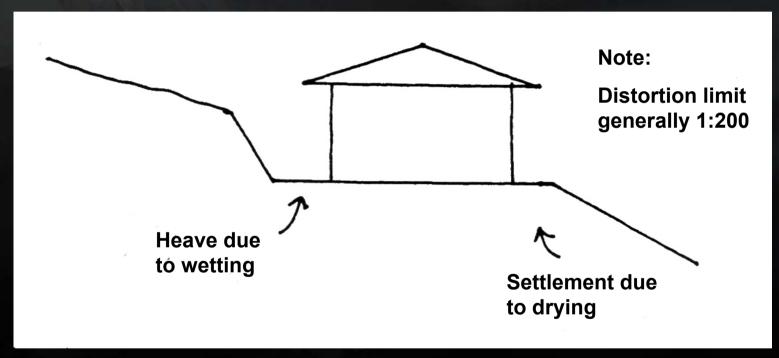


Previous structure may have changed moisture conditions



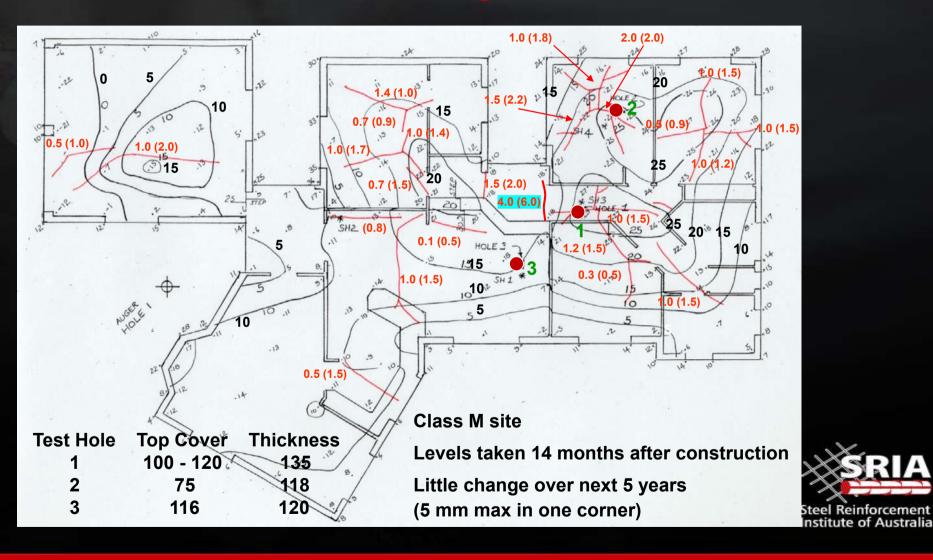
## Abnormal Moisture Conditions

#### **Cut and fill**





## Performance – Average house slab



## Table C2 of AS 2870

#### Classification of Damage with reference to concrete floors (extract)

Note: Occasional incidence of damage category 2 is expected (Cl 1.3.1)

Description of typical damage	Approx. crack width limit in floor	Change in offset from a 3 m straightedge centred over defect	Damage category
Hairline cracks, insignificant movement of slab from level (Usually no damage – Clause 1.3.1)	< 0.3 mm	< 8 mm	0 Negligible
Fine but noticeable cracks. Slab reasonably level (Low incidence of damage category 1)	< 1.0 mm	< 10 mm	1 Very slight
Cracks noticeable but easily filled.  Doors and windows stick slightly  (Occasional incidence of Category 2)	< 2.0 mm	< 15 mm	2 Slight

- **▶** How to ensure limits are achieved?
- Construct in accordance with Standard



## Construction in accordance with AS 2870?

#### Not just about placing concrete

All factors must be considered as contributing to performance

- Classify site correctly
- Select appropriate standard design
- Modify if necessary for site conditions eg rock outcrops, pipes
- Comply with detailing requirements
- Comply with construction requirements
- Unless all requirements satisfied PERFORMANCE SOLUTION



## Construction in accordance with AS 2870?

Not just about footing/raft design Walling must also be considered

#### **Articulated Masonry**

Section 3 Standard Designs include details for:

- Articulated masonry veneer
- Articulated full masonry

#### Clause 1.8.1 Articulated full masonry

Full masonry construction incorporating articulation of external and internal walls

#### Clause 1.8.2 Articulated masonry veneer

Masonry veneer construction incorporating articulation of the masonry veneer.



## **Articulated Masonry**

#### **Typical articulation joints**









## **Articulated Masonry**

#### AS 4773.1 (2015)

#### **Masonry for small buildings**

- contains requirements for articulation joints
- called up in NCC (BCA)
- contraction joints included
- expansion joints included

#### Also refer to:

CCAA TN61

**Articulated Walling** 

www.ccaa.com.au

Referenced in AS 2870

## TABLE 13.1 SPACING OF ARTICULATION JOINTS FOR UNREINFORCED MASONRY WALLS

Site class (see Note)	Masonry wall construction and surface finish	Joint spacing, m			
		Up to 4 m high for 10 mm joints	4 m to 8.5 m high for 10 mm joints	4 m to 8.5 m high for 15 mm joints	
M, M-D	External face finish masonry	6.0	4.2	6.0	
	External rendered and/or painted masonry	5.5	3.9	5.5	
	Internal face finish or sheeted masonry	6.0	4.2	6.0	
	Internal rendered and/or painted masonry	5.5	3.9	5.5	
HI, HI-D	External face finished masonry	5.5	3.9	5.5	
	External rendered and/or painted masonry	5.0	3.5	5.0	
	Internal face finish or sheeted masonry	5.5	3.9	5.5	
	Internal rendered and/or painted masonry	5.0	3.5	5.0	
H2, H2-D	External face finished masonry	5.0	3.5	5.0	
	External rendered and/or painted masonry	4.5	3.2	4.5	
	Internal face finish or sheeted masonry	5.0	3.5	5.0	
	Internal rendered and/or painted masonry	4.5	3.2	4.5	

NOTE: Site class as defined in AS 2870. For further information and guidance on site classification, see AS 2870.



## Section 5 Detailing Requirements

#### **Drainage**

#### **Requirements for rafts and slabs**

- Concrete
- Reinforcement
- Vapour barriers and damp-proofing membranes
- Edge rebates
- Recesses in slab panels
- Heating cables and pipes
- Shrinkage cracking control
- Beam continuity in rafts
- Beam layout restrictions



## Section 5 Detailing Requirements

#### **Requirements for Pad and Strip Footings**

- Concrete
- Reinforcement
- Stepping of strip footings

**Requirements in Aggressive Soils** 

Additional requirements for Classes M, H1, H2 and E Sites



## Drainage

#### Avoid water ponding against or near the footing

- Slope ground away from building (50 mm over 1 m width)
- Consider effects of a number of variables such as flooding and landscaping

#### **Avoid water entering the building**

For Class 1 buildings, minimum floor height above finished ground or paving level

- → 150 mm typically
- → 100 mm for sandy, well-drained areas
- 50 mm where adjacent paving slopes away from building
- May be reduced locally (at doorways) if shielded from weather (mandatory requirement for level access)



## Vapour Barriers & Damp-proofing Membranes

#### Materials, properties and installation

only in AS 2870 (Clause 5.3.3)

#### **NSW** and **SA**

required to have damp-proofing membrane

#### **Damp-proofing membranes**

- → Film thickness 0.2 mm
- → High impact resistance Falling Dart Test
- Resistance to puncture and moisture penetration CSIRO Test



## **Damp-proofing Membranes**

#### To ensure products meet requirements of NCC

- Obtain evidence of conformity and compliance
- Builders and inspectors should check that material supplied and installed is what has been specified in the plans and specifications
- Check that product is continuously branded as required by NCC
- Refer Advisory Notice Building 01/20 Department for Infrastructure and Transport, SA

#### **ADVISORY NOTICE** 01/20 BUILDING

Development and Infrastructure Act 2016 and the Development Act 1993

April 2020

#### TECHNICAL:

#### DAMP-PROOFING MEMBRANE REQUIREMENTS IN **SOUTH AUSTRALIA**

The purpose of this Notice is to provide information about the damp-proofing membrane requirements that apply in South Australia, the importance of these membranes complying/conforming with the requirements, and the responsibilities of the parties involved in

This Notice will also address concerns raised by the construction sector about an increasing number of non-compliant and non-con-conforming products

#### The importance of damp-proofing membranes

Buildings in South Australia are prone to rising damp and salt attack if they are not adequately protected from moisture rising from the soil below. Protection against such damage is provided through the installation of a damp proofing membranes (DPM), referred to as a vapour barrie in some States and Territories, which are laid on the ground under the concrete slab prior to the slab being poured. Diagram A indicates the location of the DPM in a typical slab-onground house. Similar products, referred to as damp-proof courses (DPCs) are also installed in walls to prevent moisture rising, however this Notice does not discuss DPC's.

If the damp-proofing products are absent or faulty, moisture can rise through the concrete slab and may have a serious, detrimental effect on the health of the occupants. As the slab becomes heavily loaded with moisture, the damp lower areas of the building can become populated with bacteria. Mould and other micro-organisms flourish in these environments and can cause allergies, asthma and irritation of the throat, eyes and skin.

A faulty DPM can allow moisture to migrate from underneath the concrete slab or from the edge of the slab into the building. If the dampness breaches the DPC in the walls it may also destroy brick work mortar joints, internal timber walls and footings. Often the first sign of a problem is damp patches on internal carpet or cupped, warped and twisted flooring or floor boards. This is often referred to as slab edge dampness (Picture A)

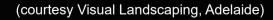


## Slab Edge Dampness - Indicators

- Persistent dampness of the exposed face
- Pungent odours in floor coverings
- Watermark stains on walls
- Mould growth
- External paint blistering/peeling below the DPC
- Delaminating (drummy) render below the DPC









(courtesy Visual Landscaping, Adelaide)



(courtesy New Home Inspections, Melbourne)

## Slab Edge Dampness

#### **Some Resources**

- 1. CCAA Data Sheet Slab Edge Dampness and Moisture Ingress
- 2. CIA Slab Edge Dampness

< DATASheet >

JAN 2005

## SLAB EDGE DAMPNESS and Moisture Ingress

#### GENERAL

The majority of houses incorporating wellconstructed and well-detailed concrete slabs and footings experience no problems with slab edge dampness. Where problems do occur, there may be no or more of several causes. A thorough investigation is required to determine the most appropriate course of action to rectify the problem.

Most slab edges are occasionally damp due to rain, garden watering or by contact with the ground. In some cases this dampness is able to permeate from the outside to the inside and affect the internal walls and/or finishes such as the floor coverings.

Preventative measures are far more effective than facing the often difficult and costly repairs required to remedy problems caused by slab edge

This data sheet explains why slab edge dampness occurs and provides recommendations to reduce the risk of moisture ingress and thus avoid the associated problems.

#### INDICATIONS OF SLAB EDGE DAMPNESS

The initial indication of a problem is usually persistent dampness of the exposed face of the concrete slab/footing, often resulting in associated efflorescence (a build up of a white coloured powdery substance) below the damp-proof course (DDC) is explained by the damp-proof course and a substance) below the damp-proof course and a substance of the dample proof o

- [DPC]. It may also result in the development of:

  upungent odours in floor coverings ie damp carpets;
- watermark stains on wall linings and/or joinery;
   mould growth:
- rusting, surface corrosion or oxidisation of metal near or adjacent to the edge of the slab/footing;
- loss of bond of adjacent wall and floor tiles;
   external paint blistering/peeling below the DPC;
- delaminating (drummy) render below the D



THE INITIAL INDICATION of a problem is usually persistent

dampness of the exposed face of

the concrete slab/footing



#### Current Practice Note 30

#### Slab Edge Dampness



#### THE PHENOMENON

Slab dege dampuess is a condition related to the serviceability of a concrete raft forcing. The major visible symptom of this condition is areas of dampuess (cometimes with efflorescence) on the slab floor internally, adjucent the perimeter walls and on the exposed odge of the footing, externally, in areas with saline such or where saline subfloor of the concrete surfaces usually follows. In South Australia the term 'slat damp' is used to describe what is broadly referred to as all attack.

Salt attack is the physical exfoliation of a concrete or masonsy surface caused by pressure exerted in surface pore spaces derived from crystalline salt growth and any phase change of salts from their anhydrous state to their hydrated state. Some of the salts fromt in soils are sulphates, chlorides, nitrates, and carbonates of sodium, calcium, maenesium and potassium.

Symptons first reported by builders and owners inside buildings are damp areas under carpets or vinyl floor coverings, with efforescence and damp slab surfaces. In more severe cases flaking or crumbly disruption of the concrete surface has also been reported. The external exposed edge of the footing often exhibits efforescence or a slaft attack type deterioration of the exposed concrete surface. Figure 1 shows the areas commonly affected by a



Figure 1 Note: (A) will usually occur if top of paving is more than around 50 mm from top of edge footing beam. (B) will usually occur if top of paving is around 50 mm or less from top of edge footing beam. (A) and (B) may occur together when top of paving is less than around 50 mm from top of edge footing.

#### SCOPE

This practice note explains the possible conditions which may cause, or contribute to, slab edge

The factors which are attributed to edge dampness to another and they may also vary around an individual site. It is not necessary for all the contributing factors to be present for shot edge dampness to occur as any one factor may cause the condition. Furthermore, one factor may not be the cause of the problem for the whole of the building.

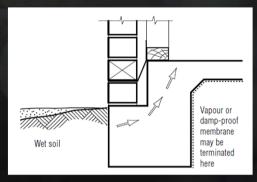
A thorough investigation of an affected property is necessary to isolate the possible cause, or causes, of slab edge dampness.

The rectification of this condition can be costly as it is usually reported after occupancy and the completion of perimeter paving. However, with sound building practice and good site supervision the occurrence of slab edge dampness can, at little cost, be dramatically reduced or eliminated.



## Slab Edge Dampness Causes and Solutions

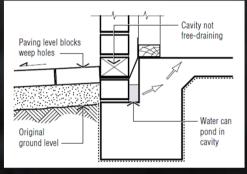
#### **Not Recommended**



Slab edge in direct contact with ground

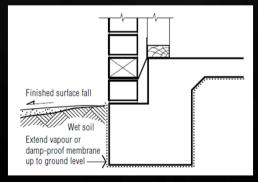
# Ground surface falls towards house Ponding, possibly also in cavity depending on the levels

Inadequate drainage

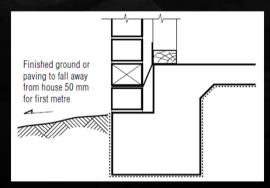


Inadequate cavity drainage

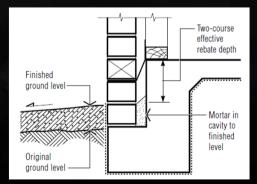
#### Recommended



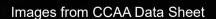
Extend vapour barrier to ground level



Free draining cavity and surrounds



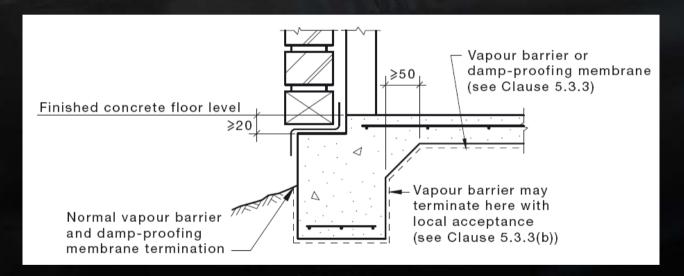
Mortar filled cavity to finished ground level





## Edge Rebates

- Minimum depth of 20 mm, except for single-leaf masonry
- Requirements for depths > 150 mm
- ➡ Where retaining > 450mm of fill refer Clause 6.4.5



Minimum rebate for cavity masonry or veneer wall (Figure 5.2(a) from AS 2870 - 2011)

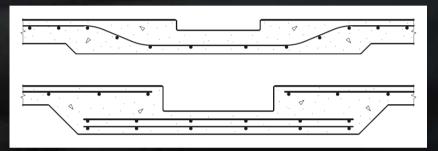


## Requirements for Rafts and Slabs

#### Recesses in slab panels

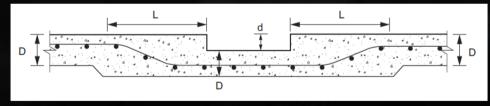
- Required slab thickness to be maintained
- Continuity of reinforcement to be maintained

Slab detail at a recess (Figure 5.3 from AS 2870 - 2011)

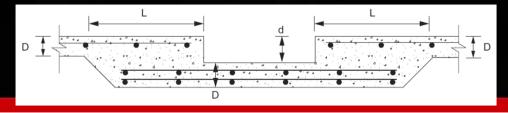


#### **Section 4.2.22 of NCC Housing Provisions Standard**

Recess depths (d) less than or equal to nominal slab thickness



Recess depths (d) greater than nominal slab thickness





## Requirements for Rafts and Slabs

#### **Shrinkage cracking control**

- ➡ Re-entrant corners 2 x 3-L8TM, 1 x 3-L11TM or 3-N12
- Brittle floor coverings
  - Minimum SL92 mesh or extra layer of slab mesh
  - Use appropriate bedding system
  - Delay placement of brittle finishes



Large tiled areas



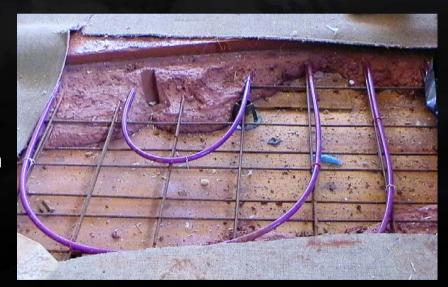
Polished concrete



## **Shrinkage cracking control – floor heating**

- ➡ Electric systems no increase in slab thickness or mesh size
- Hydronic systems
  - increase slab thickness by 25 mm
  - increase mesh by one size

Hydronic floor heating system



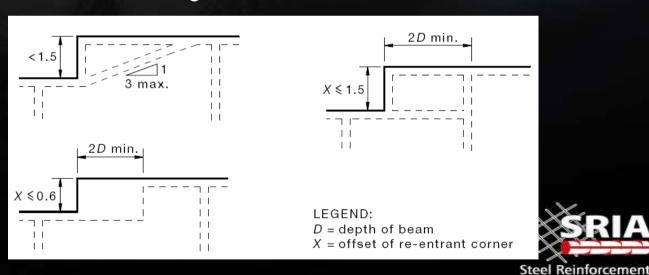


## Beam continuity in rafts

Continuity of internal and external beams must be maintained

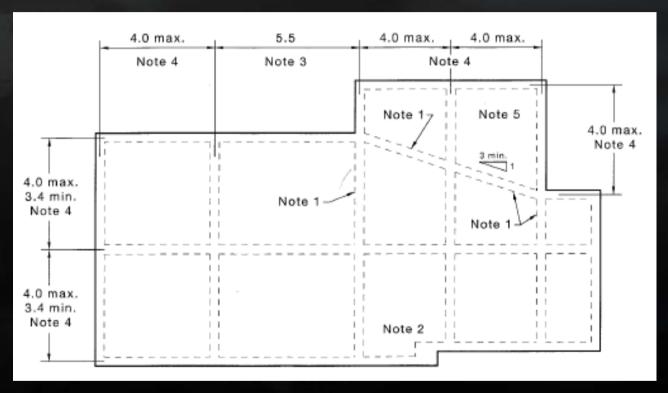
- from edge to edge of the slab
- across steps in the slab (Clause 6.4.4 (c) (iii))
- at re-entrant corners
  - provide internal beam
  - → if < 1.5 m, refer details in Figure 5.4
    </p>

Continuity of footing beams
(Figure 5.4 from AS 2870 - 2011)
(dimensions in metres)



Institute of Australia

## **Beam continuity in rafts - Commentary**



Arrangement of stiffening beams

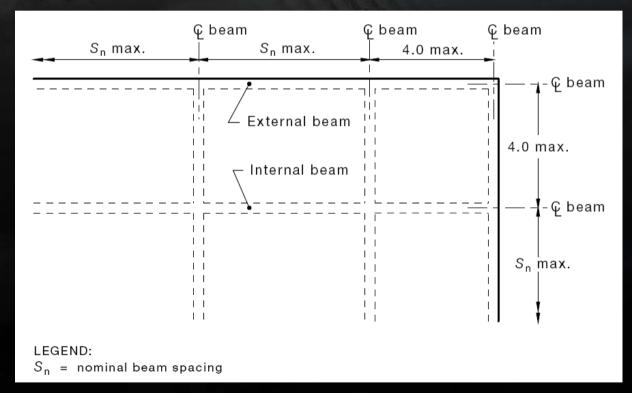
(Figure C5.4 from AS 2870 - 2011)



## **Beam layout restrictions**

Limits placed on spacing of internal beams at external corners

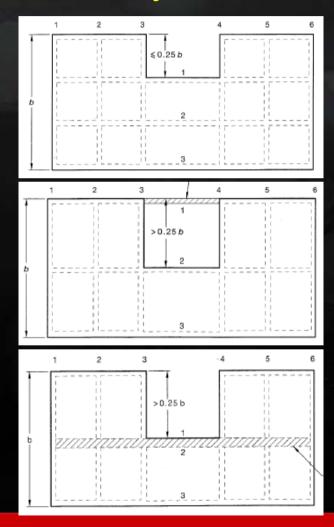
Controls deflection at external corner

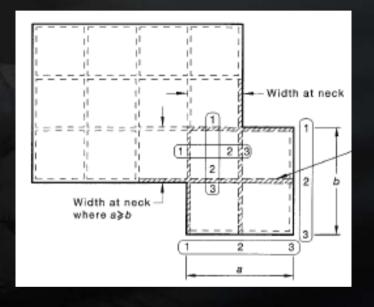




Beam spacing at external corners (Figure 5.5 from AS 2870 - 2011)

## Beam continuity in rafts – maintain stiffness





Arrangement of stiffening beams (Figure C5.5 from AS 2870 - 2011)



## **Beam continuity in rafts – maintain stiffness**

Some beams not continuous

Internal beam max. 4 m from corners?



Continue internal beam

Provide additional internal beams



## **Beam continuity in rafts – maintain stiffness**

Continue edge beam to next internal beam



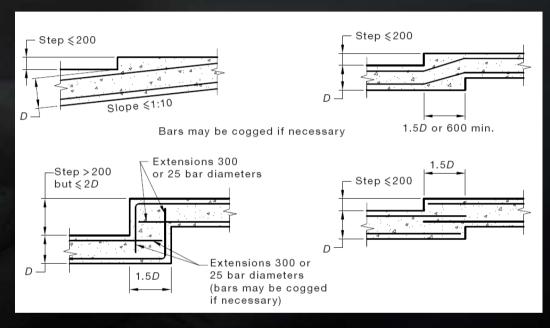


# Requirements for Pad and Strip Footings

Concrete – as for rafts and slabs

Reinforcement - covered

**Stepping of strip footings** 



Acceptable methods of stepping strip footings

(Figure 5.6 from AS 2870 - 2011)



# Cover to Reo - May be Difficult to Maintain











## Saline and sulphate soils



Western Sydney



Wagga Wagga NSW

Efflorescence is more common sign of soil salinity



Ineffective damp proof course?
Filled above damp proof course?



### **Requirements in Aggressive Soils – Clause 5.5**

#### Two choices:

- 1. Isolate the concrete or masonry member from the aggressive soil
- 2. Use appropriate concrete strength and cover

#### **Isolation of Concrete**

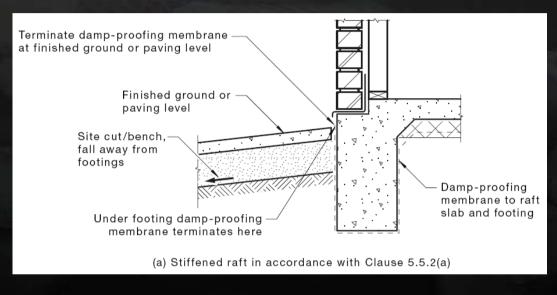
Provide damp-proofing membrane up to ground or finished paving level

- Extend membrane from under slab up to ground or paving surface
- Lap membrane from under slab with suitable damp-proofing material (0.5 mm thick) or liquid-applied waterproofing compound applied to face of concrete and extend up to finished ground or paving level





Extend membrane from under slab up to finished ground or paving level



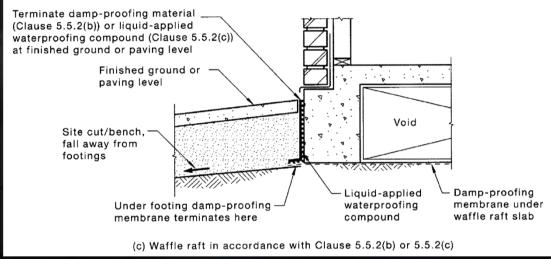


Figure 5.7 Use of damp-proofing membrane for slab protection

(from AS 2870 - 2011)



Some situations may be difficult to comply or rectify

Consider alternate edge treatments to exclude aggressive agents





## Appropriate concrete strength and detailing

Step 2 Determine required concrete strength and curing

Minimum design characteristic strength ( $f_c$ ) and curing requirements for concrete (after Table 5.3 of AS 2870 - 2011)

Exposure classification	Minimum MPa	Minimum initial curing requirement	
A1	20	Cure continuously for at least 3 days	
A2	25		
B1	32	Cure continuously for at least 7 days	
B2	40		
C1	≥50		
C2	≥50		

- **▶** Standard designs only apply to 20 and 25 MPa concrete (Clause 3.1.1 of AS 2870)
- **▶** For higher strengths, check ductility requirements



## Appropriate concrete strength and detailing

**Step 3** Determine minimum reinforcement cover

Minimum reinforcement cover for concrete (after Table 5.4 of AS 2870 - 2011)

Exposure classification	Minimum cover in saline soils	Minimum cover in sulfate soils
	(mm)	(mm)
A1	No change	40
A2	45	50
B1	50	60
B2	55	65
C1	Not applicable to salinity	70
C2	Not applicable to salinity	85

#### Concrete

- N20, 100 mm slump, 20 mm maximum nominal aggregate size
- ▶ In accordance with AS 1379 ensures quality, not final performance



## Section 6 Construction requirements

#### **Excavations**

- If permanent, retain material or batter sides
- If temporary, ensure adequate support of footings is maintained

#### Construction of slabs

- Filling controlled and rolled
- → Foundations Natural soil of 50 kPa bearing capacity for slabs
  - Natural soil of 100 kPa bearing capacity for edge footings not tied to a footing slab
  - stepping and sloping of edge beams
  - blinding layer of sand only required for aggressive soils
- Sloping Sites details of cut and fill
  - stepping of slabs and beams
  - requirements for piers



# Additional requirements for Class M, H1, H2 and E Sites

Masonry detailing – control joints

Variations in foundation material – part of footing on rock

Drainage requirements – avoid water ponding adjacent to or under footings

Plumbing requirements – Clause 5.6.4 (b) and 6.6 (e) (i)

- Penetrations through footings sleeved
- ➡ Flexible joints to drains highly and extremely reactive sites
  - commence within 1 m of the building perimeter
  - $\rightarrow$  accommodate movement up to  $y_s$  in any direction
  - be set at mid-position of their range at time of installation ie movement range of 0.5  $y_s$  from the initial setting



## Additional requirements for Class M, H1, H2 and E Sites

Flexible joints to drains (only when passing through footing?)



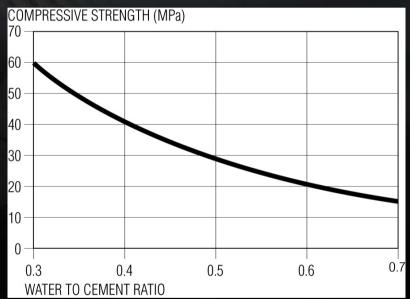




Addition of excess water on-site

Should be avoided - reduces strength





w/c ratio vs strength



### Addition of excess water on-site

- Produces Laitance/efflorescence
- May result in Flaking
- Increases risk of Cracking
  - both plastic and long-term drying shrinkage



Efflorescence



Flaking



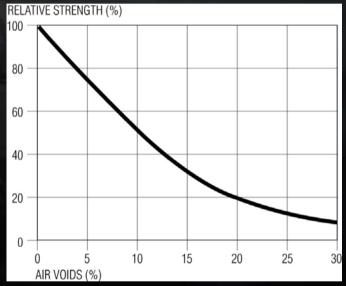
Cracking



## Compaction

Expels entrapped air – improves strength and reduces risk of cracking





Loss of Strength through incomplete compaction

## Adequate compaction

- ▶ Beams mechanically vibrate
- Slabs finishing operations satisfactory for 100 mm thickness



## Compaction

Lack of compaction reduces durability and strength

Increases risk of slab edge dampness







## Curing

- Application of water to or retention of water in concrete
- Improves strength
- Reduces permeability
- ➡ Reduces risk of cracking and crack widths









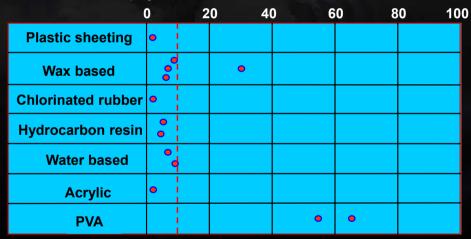
Add water to concrete (must be continuous)

Retain water in concrete



- Important for aggressive soils
   Table 5.3 Curing requirements specified
   Clause 5.5.3(d) Curing methods detailed
- Curing compounds to comply with AS 3799

72 Hour Moisture Loss (as % of untreated sample)



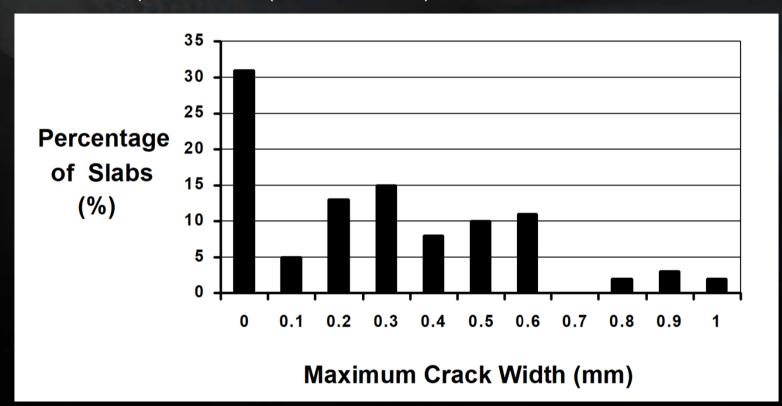
AS 3799 limit (90% retention)



## Crack Widths in residential Slabs

## Cement and Concrete Association of Australia

Technical Report TR/F129 (December 1996)

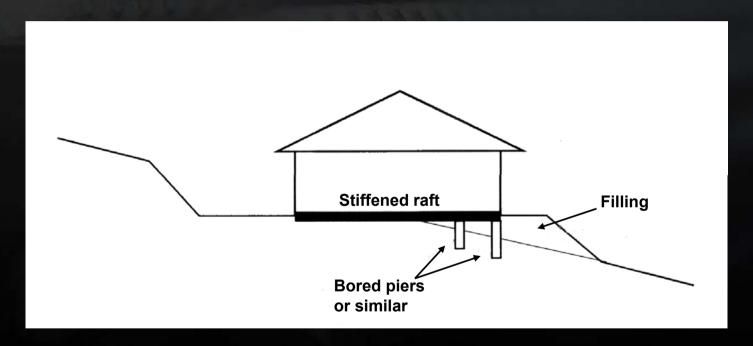




## Combined Footing Systems

Is mixed construction allowed? eg deepened footings and stiffened raft

For Class M and H sites, only one standard design shall be used (Clause 3.1.1)

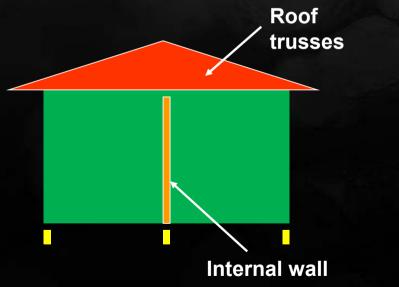


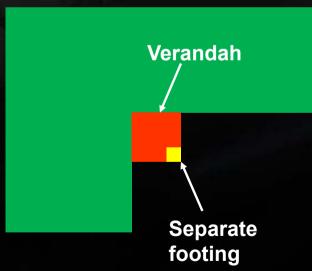


# Detailing Issues

## **Site considerations**

- Verandahs
- Trussed roofs
- Maintenance of drainage
- Gardens and watering
- Plumbing leaks







## SRIA Disclaimer

The information presented by the Steel Reinforcement Institute of Australia in this publication has been prepared for general information only and does not in any way constitute recommendations or professional advice. While every effort has been made and all reasonable care taken to ensure the accuracy of the information contained in this publication, this information should not be used or relied upon for any specific application without investigation and verification as to its accuracy, suitability and applicability by a competent professional person in this regard. The Steel Reinforcement Institute of Australia, its officers and employees and the authors and editors of this publication do not give any warranties or make any representations in relation to the information provided herein and to the extent permitted by law (a) will not be held liable or responsible in any way; and (b) expressly disclaim any liability or responsibility for any loss or damage costs or expenses incurred in connection with this publication by any person, whether that person is the purchaser of this publication or not. Without limitation, this includes loss, damage, costs and expenses incurred as a result of the negligence of the authors, editors or publishers.

The information in this publication should not be relied upon as a substitute for independent due diligence, professional or legal advice and in this regards the services of a competent professional person or persons should be sought.



# Thank you



